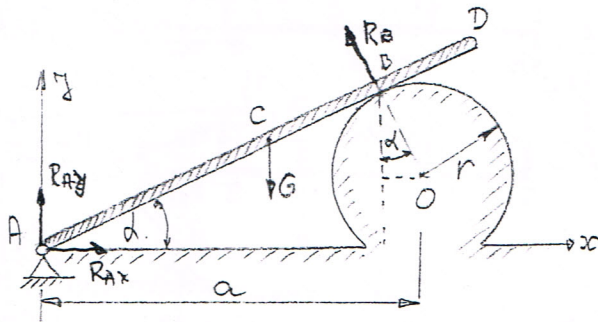


✓
 PRIMTER: STAP AD, TEŽINE G I DUBINE l , ZGLOBNO TE VEZAN U TAČKI A I U TAČKI B SE OSIĆIJA NA GLOTCI VAŽAK POLUPREČNICA r . A KO TE UGAO IZMAĐU DROVCA STAPA AD I HORIZONTALNA OSE JEDNAK α I AKO JE RASTOJAK IZ TAČKI A DO JEDNICE a ODREĐITI REAKCIJE VEZA.

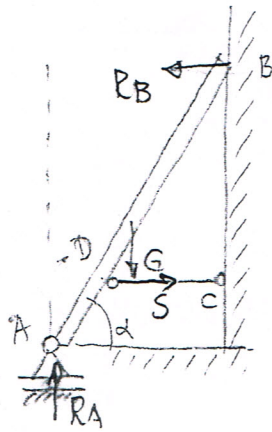


$$\sum M_A = 0: R_B \frac{(a - r \sin \alpha)}{\cos \alpha} - G \cdot \frac{l}{2} \cos \alpha = 0 \Rightarrow R_B = G \cdot \frac{1}{2} \frac{l \cos^2 \alpha}{a - r \sin \alpha}$$

$$\sum F_x = 0: R_{Ax} - R_B \sin \alpha = 0 \Rightarrow R_{Ax} = G \cdot \frac{1}{2} \frac{l \cos^2 \alpha \cdot \sin \alpha}{a - r \sin \alpha}$$

$$\sum F_y = 0: R_{Ay} - G + R_B \cos \alpha = 0 \Rightarrow R_{Ay} = G \left(1 - \frac{1}{2} \frac{l \cos^3 \alpha}{a - r \sin \alpha} \right)$$

PRIMJER: Homogeni štapa AB težine G ; dužine l oslanja se na vertikalni zid u točki B a za horizontalni pod je vezan pokretnim osloncem A. Pomocu horizontalnog veka BC štapa je vezan za zid tako da je $AD = l/6$.
 Odrediti reakcije u vezama a ko $\alpha = 60^\circ$. Zid smatramo idealno glatkim



R: $R_A = G, R_B = S = 10\sqrt{3}G$

$R_B = S$

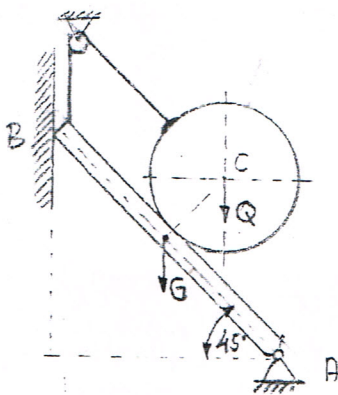
$$S \cdot \frac{l}{6} \cdot \frac{\sqrt{3}}{2} + G \cdot \frac{l}{2} \cdot \frac{1}{2} - R_B \cdot l \cdot \frac{\sqrt{3}}{2} = 0$$

$$- S \cdot l \left(\frac{\sqrt{3}}{12} - \frac{\sqrt{3}}{2} \right) = \frac{G \cdot l}{4}$$

$$S \frac{5\sqrt{3}}{12} = \frac{G \cdot l}{4} \Rightarrow S = \frac{3 \cdot G}{5\sqrt{3}} \frac{\sqrt{3}}{\sqrt{3}} = \frac{G\sqrt{3}}{5}$$

$$S = \frac{G\sqrt{3}}{5} = R_B$$

PRIMJER: Homogeni volok C, težine Q , pridržava se užetom prebačenim preko nepomičnog koturo E zanemarljive težine, vezanim u točki B. Vlak se oslanja na štapa AB, težine G i dužine l u točki na sredini štapa. Odrediti reakcije u točkama A i B, i silu u užetu.

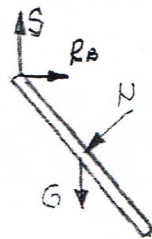
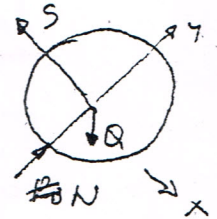


R: $R_B = Q(1 - \frac{\sqrt{2}}{2})$

$$R_{Ax} = -\frac{Q}{2}(\sqrt{2}-1)$$

$$R_{Ay} = \frac{Q}{2}(\sqrt{2}-1)$$

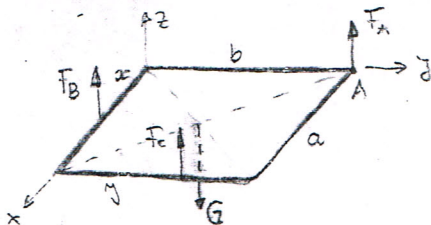
$$S = Q \cdot \frac{\sqrt{2}}{2} = N$$



$$\sum M_A = 0: S \cdot Q \cdot \frac{\sqrt{2}}{2} \cdot \frac{l\sqrt{2}}{2} + G \cdot \frac{l}{2} \cdot \frac{\sqrt{2}}{2} - Q \cdot \frac{\sqrt{2}}{2} \cdot \frac{l}{2} = 0$$

$$R_B + Q \frac{\sqrt{2}}{2} - G - \frac{Q}{2} = 0 \Rightarrow R_B = \frac{Q}{2}(\sqrt{2}-1)$$

PRIMJER: Pri dodirivanju homogene pravougaone ploče dimenzija a i b (sl), jedan od rodnica drži ploču u točki A, drugi u točki B a treći u točki C. Odrediti kolika treba da su rastojanja x i y da bi svaka od rodnica bio potpuno nako opterećen. Smatraj da su sile u točkama A, B i C vertikalne.



$$\sum M_z = 0$$

$$\sum M_x = 0: F_A \cdot b - G \cdot \frac{b}{2} + F_C \cdot y = 0$$

$$\sum M_y = 0: F_B \cdot x - G \cdot \frac{a}{2} + F_C \cdot a = 0$$

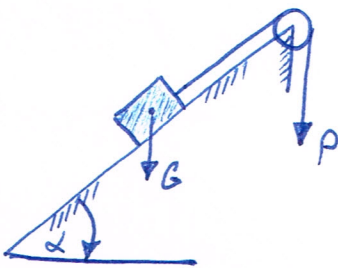
$$\sum F_x = 0$$

$$\sum F_y = 0$$

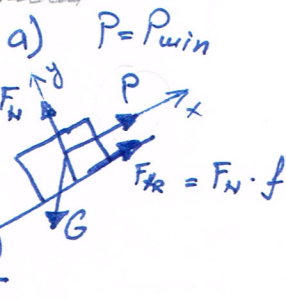
$$\sum F_z = 0: F_A + F_B + F_C - G = 0$$

Postoje $F_A = F_B = F_C$, to je $F = \frac{G}{3}, x = \frac{a}{2}; y = \frac{b}{2}$

1. Odrediti interval vrijednosti intenziteta sile P tako da tijelo težine G koje se nalazi na statnoj ravni nagiba α bude u ravnoteži. Nagib statne ravni je takav da bi se tijelo pod dejstvom sopstvene težine kretalo niz statnu ravan. Koeficijent trenja f je poznat.



1° Tijelo ima tendenciju da se kreće niz statnu ravan



$$\sum F_x = 0; P + F_{tr} - G \cdot \sin \alpha = 0$$

$$\sum F_y = 0; F_N - G \cdot \cos \alpha = 0$$

$$F_N = G \cdot \cos \alpha$$

$$P = G \cdot \sin \alpha - F_{tr}$$

$$P = G \cdot \sin \alpha - G \cdot \cos \alpha \cdot f$$

$$P_{min} = P = G (\sin \alpha - \cos \alpha \cdot f)$$

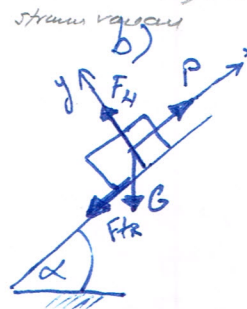
Da bi tijelo bilo u ravnoteži treba da je

$$P_{min} \leq P \leq P_{max}$$

ako je $P < P_{min}$, tijelo se kreće niz statnu ravan
a ako je $P > P_{max}$, tijelo se kreće uz statnu ravan

Razmatraćemo slučajevne kada je $P = P_{min}$ i $P = P_{max}$

2° Tijelo ima tendenciju da se kreće uz statnu ravan



$$\sum F_x = 0; P - F_{tr} - G \cdot \sin \alpha = 0$$

$$\sum F_y = 0; F_N - G \cdot \cos \alpha = 0$$

$$F_N = G \cdot \cos \alpha$$

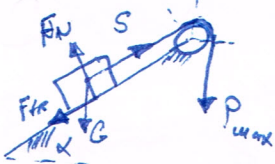
$$P_{max} = P = F_{tr} + G \cdot \sin \alpha$$

$$P_{max} = G \cdot \cos \alpha \cdot f + G \cdot \sin \alpha$$

$$P_{max} = G (\cos \alpha \cdot f + \sin \alpha)$$

$$G (\sin \alpha - \cos \alpha \cdot f) \leq P \leq G (\sin \alpha + \cos \alpha \cdot f)$$

3. Daci maksimalnu silu P_{max} , ako postoji trenje učeta o cilindričnu površ, koeficijenta k



$$P_{max} = S \cdot e^{k\theta}$$

$$F_N = G \cos \alpha$$

$$S = F_{tr} + G \sin \alpha$$

$$S = G \cos \alpha \cdot f + G \sin \alpha$$

$$P_{max} = (G (\cos \alpha \cdot f + \sin \alpha)) \cdot e^{k\theta} =$$

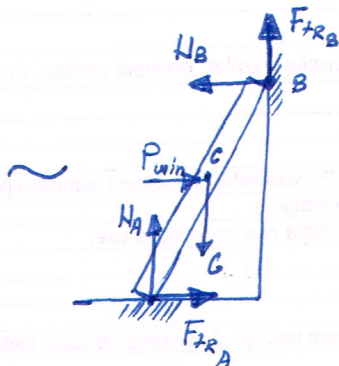
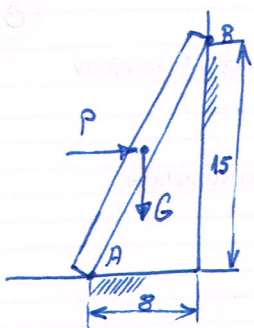
$$P_{max} = G (\cos \alpha \cdot f + \sin \alpha) \cdot e^{k(\theta + \alpha)}$$

ugao zahvata θ :
 $\theta = 90^\circ + \alpha$

2. Greda AB težine $G=10\text{ kN}$ održava se u položaju prikazanom na slici pod dejstvom sile P . Ako koeficijent trenja f na upadnim kontaktima ima vrijednost $0,2$ odrediti:

a) minimalnu vrijednost sile P da bi greda AB bila u ravnoteži

b) maksimalnu vrijednost sile P da bi greda AB bila u ravnoteži



1^o Greda ima tendenciju da se spušta pod dejstvom sile G

$$N_A = G - N_B \cdot \left(\frac{4 - 7,5f}{7,5 + 4f} \right)$$

$$\sum F_x = 0; P_{\min} + F_{trA} - N_B = 0 \dots (1)$$

$$\sum F_y = 0; N_A + F_{trB} - G = 0 \dots (2)$$

$$\sum M_C = 0; N_B \cdot 7,5 + F_{trB} \cdot 4 - N_A \cdot 4 + F_{trA} \cdot 7,5 = 0 \dots (3)$$

$$(1) \Rightarrow P_{\min} = N_B - N_A \cdot f \quad F_{trB} = N_B \cdot f$$

$$(2) \Rightarrow N_A = G - N_B \cdot f \quad F_{trA} = N_A \cdot f$$

$$(3) \Rightarrow N_B(7,5 + f \cdot 4) - N_A(4 - f \cdot 7,5) = 0$$

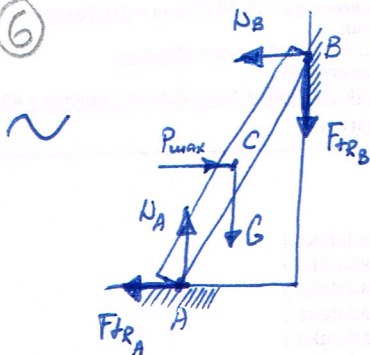
$$N_B = N_A \cdot \left(\frac{4 - 7,5f}{7,5 + 4f} \right) = 0,3 N_A$$

$$N_A = \frac{G}{1 + \left(\frac{4 - 7,5f}{7,5 + 4f} \right) \cdot f} = 9,43 \text{ kN}$$

$$N_B = 2,8 \text{ kN}; \quad P_{\min} = 1 \text{ kN}$$

$$P_{\min} = N_B - N_A \cdot f = 2,8 - 9,43 \cdot 0,2 = 0,91$$

6



2^o Greda ima tendenciju da se podiže pod dejstvom sile P

$$\sum F_x = 0; P_{\max} - F_{trA} - N_B = 0 \dots (1)$$

$$\sum F_y = 0; N_A - G - F_{trB} = 0 \dots (2)$$

$$\sum M_C = 0; N_B \cdot 7,5 - F_{trB} \cdot 4 - N_A \cdot 4 - F_{trA} \cdot 7,5 = 0 \dots (3)$$

$$N_B(7,5 - 4 \cdot f) - N_A(4 + 7,5 \cdot f) = 0$$

$$N_B = N_A \cdot \frac{4 + 7,5f}{7,5 - 4 \cdot f}$$

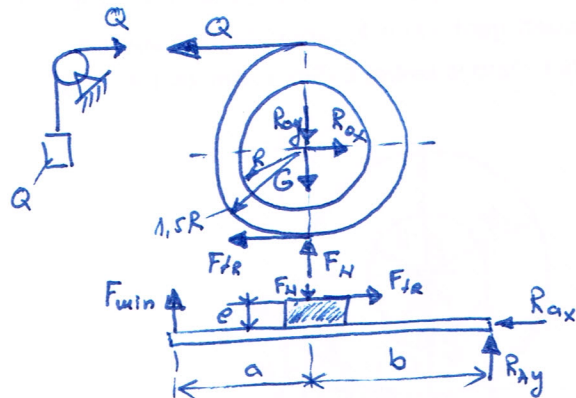
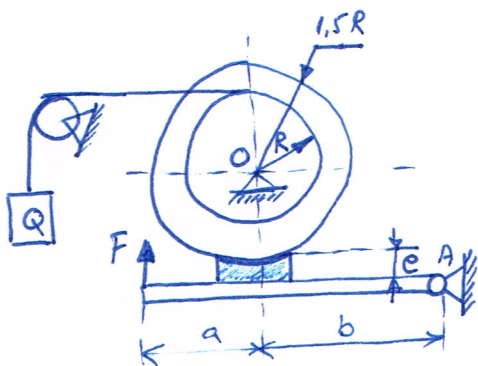
$$N_A = G + N_B \cdot f$$

$$N_A = \frac{G}{1 - \frac{4 + 7,5f}{7,5 - 4 \cdot f} \cdot f} = 12 \text{ kN}$$

$$N_B = 10,0 \text{ kN}; \quad P_{\max} = 12,4 \text{ kN}$$

$$N_B = \frac{N_A - G}{f}; \quad P_{\max} = N_B + N_A \cdot f$$

3. Odrediti minimalnu vrijednost sile F , reakcije u osloncima A i O i silu međusobnog pritiska između papuče kočnice i koalsijalnog doboša kočnice prikazane na slici. Težina štapa AB se zanemaruje, dok su težine tečeta i doboša Q , odnosno G . Koefficient trenja između papuče i doboša je f_0 . Ostali potrebni podaci dati su na slici.



Doboš:

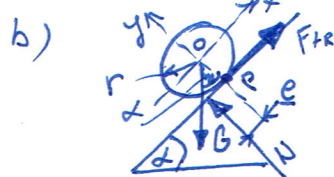
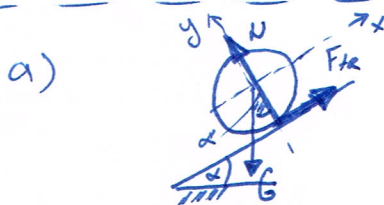
$$\begin{aligned} \Sigma M_O = 0; & F_{tr} \cdot 1.5 \cdot R - Q \cdot R = 0 \Rightarrow F_{tr} = F_N \cdot f_0; \quad \boxed{F_N = \frac{Q}{1.5 \cdot f_0}} \\ \Sigma F_x = 0; & R_{ox} - Q - F_{tr} = 0; \Rightarrow R_{ox} = Q + F_N \cdot f_0; \quad \boxed{R_{ox} = \frac{5}{3} Q} \\ \Sigma F_y = 0; & F_N - R_{oy} - G = 0; \quad R_{oy} = F_N - G \Rightarrow \boxed{R_{oy} = \frac{2 \cdot Q}{3 \cdot f_0} - G} \end{aligned}$$

POLUGA:

$$\begin{aligned} \Sigma M_A = 0; & F_{min}(a+b) + F_{tr} \cdot e - F_N \cdot b = 0; \Rightarrow F_{min} = (F_N \cdot b - F_{tr} \cdot e) \cdot \frac{1}{a+b} = \frac{2}{3} Q \cdot \frac{b - e \cdot f_0}{(a+b) \cdot f_0} \\ \Sigma F_x = 0; & F_{tr} - R_{ax} = 0 \Rightarrow \boxed{R_{ax} = \frac{2}{3} Q} \\ \Sigma F_y = 0; & F_{min} + R_{ay} - F_N = 0 \Rightarrow \boxed{R_{ay} = \frac{2}{3} Q \cdot \frac{a + e \cdot f_0}{(a+b) \cdot f_0}} \end{aligned}$$

4. Točak poluprecnika r , se nalazi na stanoj ravni nagibnog ugla α i koefficienta trenja μ . Odrediti:

- ugao α , tako da dođe do klizanja točka
- krak trenja kotrljanja e , tako da dođe do kotrljanja točka



(1) $\Sigma F_x = 0; F_{tr} - G \cdot \sin \alpha = 0; F_{tr} = N \cdot \mu$

(2) $\Sigma F_y = 0; N - G \cdot \cos \alpha = 0$

$$\left. \begin{aligned} (1) \Rightarrow N &= \frac{G \cdot \sin \alpha}{\mu} \\ (2) \Rightarrow N &= G \cdot \cos \alpha \end{aligned} \right\} \begin{aligned} G \cdot \cos \alpha \cdot \mu &= G \cdot \sin \alpha \\ \mu &= \tan \alpha \end{aligned}$$

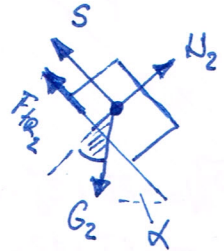
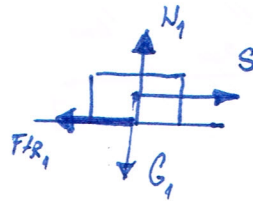
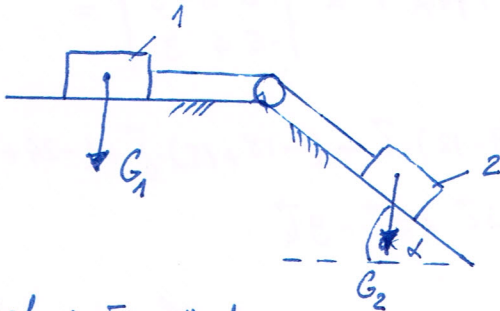
(1)... $\Sigma F_y = 0; N - G \cdot \cos \alpha = 0; \Rightarrow N = G \cdot \cos \alpha$

(2)... $\Sigma M_P = 0; N \cdot e - G \cdot \sin \alpha \cdot r = 0$

$$G \cdot \cos \alpha \cdot e = G \cdot \sin \alpha \cdot r$$

$$\boxed{e = \tan \alpha \cdot r}$$

5. Dva tijela težina G_1 i G_2 vezana su nerastopljivim užetom. Odrediti težinu tijela u stanju ravni, da bi sistem bio u stanju uirovanja. Dato je: $G_1 = 10 \text{ kN}$; $f_1 = 0,1$; $f_2 = 0,2$; $\alpha = 30^\circ$. Trenje uzeta o cilindričnu površ zanemariti.



$$F_{fr_1} = N_1 \cdot f_1; \quad F_{fr_2} = N_2 \cdot f_2$$

tijelo 1:

$$\sum F_y = 0; \quad N_1 - G_1 = 0$$

$$N_1 = G_1$$

$$\sum F_x = 0;$$

$$S - F_{fr_1} = 0$$

$$S = F_{fr_1}$$

$$S = N_1 \cdot f_1 = G_1 \cdot f_1$$

tijelo 2:

$$\sum F_y = 0; \quad N_2 - G_2 \cdot \cos \alpha = 0$$

$$N_2 = G_2 \cdot \cos \alpha$$

$$\sum F_x = 0; \quad G_2 \cdot \sin \alpha - S - F_{fr_2} = 0$$

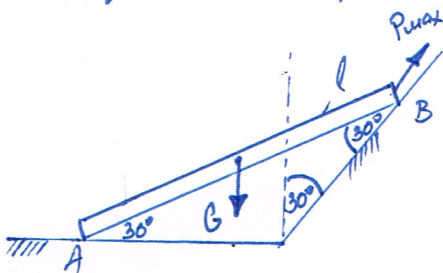
$$G_2 \cdot \sin \alpha - G_1 \cdot f_1 - N_2 \cdot f_2 = 0$$

$$G_2 \cdot \sin \alpha - G_1 \cdot f_1 - G_2 \cdot \cos \alpha \cdot f_2 = 0$$

$$G_2 (\sin \alpha - \cos \alpha \cdot f_2) = G_1 \cdot f_1$$

$$G_2 = \frac{G_1 \cdot f_1}{\sin \alpha - \cos \alpha \cdot f_2} = \frac{10 \cdot 0,1}{\sin 30^\circ - \cos 30^\circ \cdot 0,2} \approx 3 \text{ kN}$$

6. Za gredicu dužine l i težine G , u položaju prikazanom na slici, odrediti maksimalnu vrijednost sile P da bi tijelo bilo u stanju uirovanja. Koefficient trenja između grede i horizontalne podloge je f .



$$\sum F_x = 0; \quad P_{\max} \cdot \sin 30^\circ - F_{fr} - N_2 \cdot \cos 30^\circ = 0$$

$$\sum F_y = 0; \quad N_1 + P_{\max} \cdot \cos 30^\circ - G + N_2 \cdot \sin 30^\circ = 0$$

$$(1) \quad \sum M_B = 0; \quad N_1 \cdot \frac{\sqrt{3}}{2} + N_1 \cdot f \cdot \frac{l}{2} - G \cdot \frac{\sqrt{3}}{2} \cdot \frac{1}{2} = 0$$

$$(2) \quad \sum M_A = 0; \quad P \cdot l - N_1 \cdot f \cdot l - G \cdot \frac{\sqrt{3}}{2} \cdot \frac{1}{2} = 0$$

$$(1) \Rightarrow \frac{N_1}{2} (f + \sqrt{3}) = \frac{G\sqrt{3}}{4}; \quad N_1 = \frac{\sqrt{3}}{2(\sqrt{3}+f)} \cdot G$$

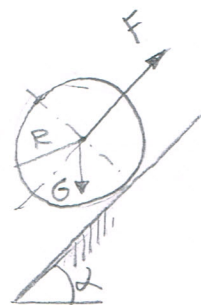
$$(2) \Rightarrow P = N_1 \cdot f + \frac{G\sqrt{3}}{4}$$

$$P = \frac{G\sqrt{3} \cdot f}{2 \cdot (\sqrt{3}+f)} + \frac{G\sqrt{3}}{4} = \frac{G\sqrt{3}}{4} \left(\frac{2f}{\sqrt{3}+f} + 1 \right) = \frac{G\sqrt{3}}{4} \left(\frac{2f + \sqrt{3} + f}{\sqrt{3}+f} \right)$$

$$P = \frac{G\sqrt{3}}{4} \left(\frac{3f + \sqrt{3}}{f + \sqrt{3}} \right)$$

$$F_{fr} = N_1 \cdot f$$

TOČAK POLUPREČNIKA R [m] I MASE m [kg] SE
 NALAZI NA STROMJ PAVNI NAGIBNOG UGLA α .
 KOEFICIJENTI TREŃJA KLIZANJA I KOTRANJA
 SU: f ; e [m].



ODREĐITI VELEČINOSTI SILE F TAKO DA TOČAK
 KLIZA A NEKOTRJA NA STROMJ PAVAN
 UČETI: $R=0,4$ m ; $m=80$ kg ; $\alpha=45^\circ$; $f=0,2$; $e=0,3$ m

$g=10 \text{ m/s}^2$

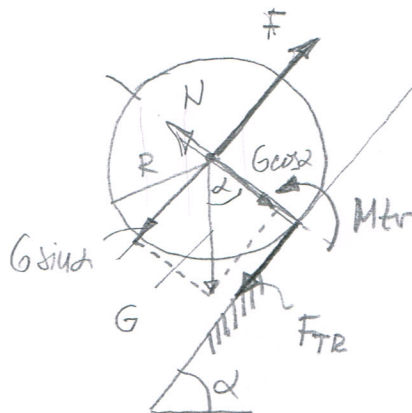
$G = 80 \cdot 10 = 800 \text{ N}$

$F_{Tr} = N \cdot f$

$N = G \cos \alpha = 800 \cdot \frac{\sqrt{2}}{2} = 400\sqrt{2} \text{ N}$

$F_{Tr} = 400\sqrt{2} \cdot 0,2 = 80\sqrt{2} \text{ [N]} = 113,1 \text{ N}$

$M_{Tr} = N \cdot e = 400\sqrt{2} \cdot 0,3 = 120\sqrt{2} \text{ [N]} = 169,7 \text{ Nm}$



KLIZA UZ

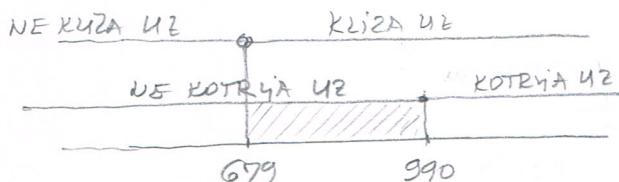
$F > G \sin \alpha + F_{Tr}$

$F > 800 \cdot \frac{\sqrt{2}}{2} + 80\sqrt{2} = 480\sqrt{2} = 679 \text{ N}$

NE KOTRJA UZ

$F \cdot R \leq G \sin \alpha \cdot R + M_{Tr} = G \sin \alpha \cdot R + N e$

$F \leq G \sin \alpha + \frac{N e}{R} = \frac{800 \cdot \frac{\sqrt{2}}{2} + 120\sqrt{2}}{0,4} = 900\sqrt{2} = 990 \text{ N}$



$F \in (679, 990]$ - KLIZA A NE KOTRJA UZ STROMJ PAVAN

$F \in [-\infty, 679]$ - NE KLIZA I NE KOTRJA UZ STROMJ PAVAN

$F \in [990, \infty]$ - KLIZA I KOTRJA UZ STROMJ PAVAN